# EEE 472 POWER SYSTEM ANALYSIS II Symmetrical Fault Analysis (Balanced 3-Phase Faults) Z<sub>bus</sub> Method

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- In a large network, an impedance matrix is readily available
- Matrix algebra formation
  - Seek a matrix where the diagonal elements represent the source impedance for the buses
- Consider the following system



Balanced operation is assumed

Place the prefault voltages into a vector

$$V_{bus}(0) = \begin{bmatrix} V_1(0) & \cdots & V_k(0) & \cdots & V_n(0) \end{bmatrix}^T$$

Replace the loads by a constant impedance model using the prefault bus voltages

$$Z_i = \frac{\left| V_i \left( 0 \right) \right|^2}{S_i^*}$$

The voltage change(\Delta V) is determined by placing a fault voltage at the faulted bus with all the other sources short-circuited



Superposition: the fault voltages are calculated from the prefault voltages

$$\mathbf{V}_{\text{bus}}^{\text{f}} = \mathbf{V}_{\text{bus}}(0) + \Delta \mathbf{V}_{\text{bus}}$$

where bus voltage changes caused by the fauly

$$\Delta \mathbf{V}_{\text{bus}} = \begin{bmatrix} \Delta \mathbf{V}_1 & \cdots & \Delta \mathbf{V}_k & \cdots & \Delta \mathbf{V}_n \end{bmatrix}^{\mathrm{T}}$$

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The change in bus voltages can be calculated from the network matrix

$$\begin{bmatrix} 0\\ \vdots\\ -I_k(F)\\ \vdots\\ 0 \end{bmatrix} = \begin{bmatrix} Y_{11} & \cdots & Y_{1k} & \cdots & Y_{1n}\\ \vdots\\ Y_{k1} & \cdots & Y_{kk} & \cdots & Y_{kn}\\ \vdots\\ Y_{n1} & \cdots & Y_{nk} & \cdots & Y_{nn} \end{bmatrix} \begin{bmatrix} \Delta V_1\\ \vdots\\ \Delta V_k\\ \vdots\\ \Delta V_k\\ \vdots\\ \Delta V_n \end{bmatrix}$$

$$\mathbf{I}_{bus}(F) = \mathbf{Y}_{bus} \mathbf{\Delta} \mathbf{V}_{bus}$$

Solving for bus voltage changes

$$\mathbf{\Delta V}_{bus} = \mathbf{Z}_{bus} \mathbf{I}_{bus}(F)$$

$$\mathbf{Z}_{bus} = \mathbf{Y}_{bus}^{-1}$$

The bus voltages during the fault:

$$\mathbf{V}_{bus}(F) = \mathbf{V}_{bus}(0) + \mathbf{Z}_{bus}\mathbf{I}_{bus}(F)$$

$$\begin{bmatrix} V_1(F) \\ \vdots \\ V_k(F) \\ \vdots \\ V_n(F) \end{bmatrix} = \begin{bmatrix} V_1(0) \\ \vdots \\ V_k(0) \\ \vdots \\ V_n(0) \end{bmatrix} + \begin{bmatrix} Z_{11} & \cdots & Z_{1k} & \cdots & Z_{1n} \\ \vdots & \vdots & \vdots & \vdots & \vdots \\ Z_{k1} & \cdots & Z_{kk} & \cdots & Z_{kn} \\ \vdots & \vdots & \vdots & \vdots & \vdots \\ Z_{n1} & \cdots & Z_{nk} & \cdots & Z_{nn} \end{bmatrix} \begin{bmatrix} 0 \\ \vdots \\ -I_k(F) \\ \vdots \\ 0 \end{bmatrix}$$

$$V_k(F) = V_k(0) - Z_{kk}I_k(F)$$

$$V_k(F) = Z_fI_k(F)$$

$$I_k(F) = \frac{V_k(0)}{Z_{kk} + Z_f}$$

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The bus voltage during the fault at bus i becomes

$$V_{i}(F) = V_{i}(0) - Z_{ik}I_{k}(F)$$

$$I_{k}(F) = \frac{V_{k}(0)}{Z_{kk} + Z_{f}}$$

$$V_{i}(F) = V_{i}(0) - \frac{Z_{ik}}{Z_{kk} + Z_{f}}V_{k}(0)$$

- Note that for bolted fault  $Z_f = 0$  and  $V_k(F) = 0$
- With the knowledge of bus voltages during the fault, we can calculate the current in all the lines. For the line connecting bus *i* and *j* with impedance z<sub>ij</sub>, the short-circuit current in this line

$$I_{ij}(F) = \frac{V_i(F) - V_j(F)}{z_{ij}}$$

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# Example 1 (cont'd)

#### 3-phase fault with Z<sub>f</sub> = j0.16 on



#### Example 1 (cont'd)



 $V_1(F) = V_1(0) - Z_{13}I_3(F) = 1.0 - (j0.12)(-j2.0) = 0.76 \text{ pu}$   $V_2(F) = V_2(0) - Z_{23}I_3(F) = 1.0 - (j0.16)(-j2.0) = 0.68 \text{ pu}$  $V_3(F) = V_3(0) - Z_{33}I_3(F) = 1.0 - (j0.34)(-j2.0) = 0.32 \text{ pu}$ 

$$I_{12}(F) = \frac{V_1(F) - V_2(F)}{z_{12}} = \frac{0.76 - 0.68}{j0.8} = -j0.1 \text{ pu}$$
$$I_{13}(F) = \frac{V_1(F) - V_3(F)}{z_{13}} = \frac{0.76 - 0.32}{j0.4} = -j1.1 \text{ pu}$$
$$I_{23}(F) = \frac{V_2(F) - V_3(F)}{z_{23}} = \frac{0.68 - 0.32}{j0.4} = -j0.9 \text{ pu}$$

11

#### A 3-phase fault occurs at bus 2



#### **Example 2-Solution**

Fault current

$$I_f = V_f / Z_{22} = 1.0 / j.2295 = -j4.3573 p.u.$$

Voltages during fault

$$\begin{bmatrix} V_1 \\ V_2 \\ V_3 \\ V_4 \end{bmatrix} = \begin{bmatrix} 1 - j0.1938 / j0.2295 \\ 0 \\ 1 - j0.1494 / j0.2295 \\ 1 - j0.1506 / j0.2295 \end{bmatrix} = \begin{bmatrix} 0.1556 \\ 0 \\ 0.3490 \\ 0.3438 \end{bmatrix}$$

Fault currents contributed to bus 2

From bus 1 I<sub>f1</sub> = V<sub>1</sub> / Z<sub>b1</sub> = 0.1556 / j0.125 = -j1.2448 p.u.
 From bus 3 I<sub>f3</sub> = V<sub>3</sub> / Z<sub>b3</sub> = 0.3490 / j0.25 = -j1.3960 p.u.
 From bus 4 I<sub>f4</sub> = V<sub>4</sub> / Z<sub>b4</sub> = 0.3438 / j0.20 = -j1.7190 p.u.

3. A three-phase fault occurs at the receiving end of the transmission line. By ignoring the pre-fault loading conditions, find the fault current using Z-bus method. (Choose  $V_B=30 \text{ kV}$  of the generator voltage and  $S_B = 100 \text{ MVA}$ ) (25 pts)



#### **Example 3-Solution**

 $X_{62} = j_{0.24} \left( \frac{100}{40} \right) = j_{0.6} p_{4} p_{4}$   $X_{7} = j_{0.16} p_{4} (\frac{100}{40}) = j_{0.6} p_{4} p_{4}$   $Z_{7} = j_{0.16} p_{4} (\frac{100}{40}) = j_{0.6} p_{4} p_{4}$   $Z_{7} = j_{0.16} p_{4} (\frac{100}{40}) = j_{0.6} p_{4} p_{4} (\frac{100}{40}) = j_{0.24} p_{4} (\frac{100}$  $-\frac{30.4}{30.6} -\frac{30.4}{30.1} = \frac{100}{30.6} = \frac{100}{30.1} = \frac{100}{30.5} = \frac{100}{5} =$ ZBUS = YRIN  $|Y_{310}| = -30.818 + 14.792$ = -16.026 (5)

The figure given below shows a generating station feeding a 220 kV system. Determine total fault current and fault current supplied by each generator for a three-phase fault at the receiving end of the line.



G1: 11 KV, 100 MVA,  $x'_{g1} = j0.15$ 

 $G_2$ : 11 KV, 75 MVA,  $x'_{g_2} = j0.125$ 

T1: 100 MVA,  $x_{T1} = j0.10, 11/220$  KV

$$T2$$
: 75 MVA,  $x_{T2} = j_{0.08}, 11/220$  KV

 $y_{3} = \frac{1}{x_{3}} = -j23.041 \text{ pu}$   $y_{3} = \frac{1}{x_{3}} = -j23.041 \text{ pu}$   $y_{3} = \frac{1}{x_{3}} = -j23.041 \text{ pu}$   $y_{3} = \frac{1}{y_{3}} = -j23.041 \text{ pu}$ Let SR = 100 mun, UB = 11KU Xp1 = j0.15pu,  $x_{g_2} = j0.125 \left(\frac{100}{75}\right) = j0.167 py$ XTI = 30.10 pu  $2_{BUD} = \gamma_{BUS} = j_{0.131} j_{0.134} j_{0.134}$  $X_{T2} = j_{0,08} \left( \frac{100}{75} \right) = j_{0,107} p_{10}$  $2B = \frac{V_B^2}{S_B} = \frac{220^2}{100} = 484 \Omega^2$ The fourt Current:  $X_{Line} = \frac{j42}{484} = j0.0868 p4$  $\frac{700000}{100000} = \frac{3-phayle}{3-phayle} I_{f} = \frac{V_{f}}{222} = \frac{1.0}{j0.174} = -\frac{15.75pu}{5}$ - $\frac{700-7}{50.0368} = \frac{700\times10^{6}}{100\times10^{6}} = 262.43.4$ Igif 2001 230.158 30.167 |If | = 5.75x 262.43 = 1508.98A. A-192F  $v'_{1} = 1 - \frac{212}{322} = 1 - \frac{j_{0,13}!}{j_{0,17}!} = 0.247$   $v'_{2} = 0 - \frac{1 - 0.247}{1 - 0.247} = -j_{3,01274}$ X1= 20.1+ 20.15= 20.25 pu  $y_i = \frac{1}{x_i} = -j4 pu$  $X_2 = j0.167 + j0.107 = j0.274P41$  $I_{glf} = jo.25$  $\hat{I}_{g2f} = \frac{1-0.247}{j0.274} = -j2.748 p_4$  $y_2 = \frac{1}{X_2} = -j3.65 pu$  $T_{B} = \frac{100 \times 10^{6}}{\sqrt{3} \times 11 \times 10^{3}} = 5248.645$   $F_{9c}fl = 14.423$ X3 = j0.0868/130.0868 = 10.0434 PU 120mpl- BICILY 5048 = 1518 KA

#### Example 4 Solution

- For the three-bus system given below, a three-phase fault occurs at bus # 3. By ignoring the pre-fault loading conditions and using the Zbus (bus impedance) method, compute the followings:
  - Fault current (15)
  - Bus voltages during the fault (10)
  - Fault currents of lines and generators(10)



#### **Example 5-Solution**

 $Y_{B} = \begin{bmatrix} -j_{12} & j5 & j5 \\ j5 & -j_{12} & j5 \\ j5 & j5 & -j_{10} \end{bmatrix}$ Lines and generators fault c) $\mathcal{F}_{B} = Y_{B} = \begin{bmatrix} j_{0}, 2793 & j_{0}, 2204 & j_{0}, 25 \\ j_{0}, 2206 & j_{0}, 2793 & j_{0}, 25 \\ j_{0}, 256 & j_{0}, 25 \end{bmatrix} \begin{bmatrix} currents : \\ gonoring & pre-fault & logding \\ fonoring & pre-fault & logding \\ condition : \\ j_{0}, 25 & j_{0}, 25 & j_{0}, 35 \\ logding & logding \\ logding$ currents :  $I_{GI} = \frac{1.0 - 0.2357}{j0.5} - j1.4286pu$ 9) Fault current  $\overline{I_{f}} = \frac{1.0}{j0.35} = -j^{2.857} p_{H} \qquad \overline{I_{62}} = \frac{1.0 - 0.2857}{+j0.5} = -j1.4286 p_{H} \qquad p_{H} \qquad \overline{I_{12}} = \frac{0.2857 - 0.2857}{-j0.2} = 0 p_{H} \qquad p_{H}$ -0.35  $b) \quad v_{1}' = 1 - \frac{2}{233} = 1 - \frac{j0.25}{j0.35}$   $I_{12} = \frac{0.2857 - 0.2857}{j0.2} = 0$   $I_{3} = \frac{0.2857 - 0}{j0.2} = -j1.428$   $I_{3} = \frac{0.2857 - 0}{j0.2} = -j1.428$   $I_{23} = \frac{0.2857 - 0}{j0.2} = -j1.4285$   $I_{23} = \frac{0.2857 - 0}{j0.2} = -j1.4285$ 1.0 10  $V_2 = 0.2857 P4$ V3 = 0 pu

The two-bus system below provides power to the motor when the voltage of the bus 1 is  $V_1 = 0.9 \angle 0^0$  pu and the generator current is  $I_G = 1.0 \angle 36.87^0$  pu. A threephase fault occurs at bus 2. Using the Z-bus matrix (bus impedance matrix) find the fault current, the contribution of the generator and the motor to the fault current and bus voltages during the fault (35 p)



#### **Example 6-Solution**



#### **Example 6-Solution**

The fault current VF = 0.963 [-4.76 722 j0.146 -=6.596]-94.76 PY Bus voltage during fault:  $=V_{1}-I_{f}^{2}$ ·(j0.087  $V_{i} = 0.331 \lfloor 8.25^{\circ} PU$ r 160

The contribution of the penerator and the motor to the fault arrest: 8.25-0 .j 0.1 = 3.31 - 81.75°  $= I_{c} + I_{m}$ Im = 6.5961-94.76 - 3.31)-81.75, n = 3.45 | -113.72 py



A three-bus power system is shown above. The p.u. impedances are on a base of 50 MVA and 12 kV. A three-phase symmetrical short circuit occurs at bus 3 with no fault impedance. Using Z-bus matrix method and ignoring pre-fault loading conditions:

- a) Compute the short-circuit current (20)
- b) Bus voltages during fault (5)
- c) Contributions of generators to the short-circuit current (5)

#### **Example 7-Solution**

Joit - 110 -j13.33 0.1 -j6.67 1.0  $\sim$ Г-j26.67 ў10 ў10 j10 -j33.33 ў10 j10 ў10 -j20 Ybus = 0) 0.05571 0.03857  $\Xi_{bub} = [Y_{bub}]^{-1} = j \begin{bmatrix} 0.07286 \\ 0.03857 \\ 0.05571 \end{bmatrix}$ 0.04714 0.05571 0.10143 0.04714

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#### **Example 7-Solution (cont'nd)**

$$\frac{short \ circuit \ a + bu5 \ 3}{I_{3f}} = \frac{1}{j0.10143} = -j9.86 \ PU}$$
Bare current  $I_{B} = \frac{50 \times 10}{\sqrt{3} (12 \times 10^{3})} = 2405.6 \ A$  (10)  
Fould current  $I_{3f} = (-j9.86)(2405.6) = -j23.72 \ KA$   
b)  $V_{1} = 1.0 - \frac{213}{233} = 1.0 - \frac{j0.0557}{j0.10143} = 0.451 \ PU$   
 $V_{2} = 1.0 - \frac{223}{233} = 4.0 - \frac{j0.04714}{j0.10143} = 0.535 \ PU$   
 $V_{3} = 0 \ PU$   
c)  $I_{G_{1}} = \frac{1 - 0.451}{j0.15} = -j3.66 \ PU \ OT$   
 $I_{G_{2}} = \frac{1 - 0.451}{j0.075} = -j6.2 \ PU$   
 $I_{G_{2}} = \frac{1 - 0.535}{j0.075} = -j6.2 \ PU$   
 $I_{G_{2}} = (-j6.2)(2405.6) = -j14.91 \ KA$ 

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